



Estruturas Aeroespaciais I – 10362/15089

2023/2024

Mini Project Sizing of a wingbox

1. OBJECTIVE

To size the structure of a wingbox subject to strength and stiffness constraints. To write a technical report.

2. DESCRIPTION

It is required to size the wingbox of a two-seat general aircraft which has a maximum take-off mass of m = 750 kg and limit load factors of n = +4/-2.

A simplified representation of the wing's geometry and the definition of the wingbox parameters are shown in Figure 1. The wingbox has a constant width 0.3c, a constant height h, and a span b.

The wingbox structure is made of a closed thin-walled single section. The wingbox skin has thickness t_c and the spar web has thickness t_a . The cross-section areas of the upper and lower spar flanges are A_l and A_2 , respectively. These areas are made of L sections of equal sized sides, d_i , and thickness t_i (i=1,2). The root of the wing is assumed to be built-in at the main spar and the tip is free. One of three different materials can be used in the design of the wingbox, the aluminium alloys 7075-T6, 2024-T3 or 6061-T6, all being isotropic materials with properties given in Table 1. The available material thicknesses are given in Table 2.

A first load case to apply to the wing includes a uniformly distributed vertical load, w_L , along the span corresponding to the wing lift and a uniformly distributed torsion moment, w_T , along the span. This load system is applied a distance 0.05c in front of the wing spar at the horizontal symmetry axis. A second load case has an upward point force acting on the spar at a distance 1.6 m from the wing root. This force represents the ground reaction at the main wheel in a landing condition with a ground load factor $n_g = 3.5$.

The maximum lift coefficient of the wing is $C_{Lmax} = 1.66$, the minimum negative lift coefficient is $C_{Lmin} = -C_{Lmax}/2$, the lift coefficient is given by $C_L = 0.011 \pi^2 b(\alpha + 4)/(b + 2c)$, where α is the angle of attack, the pitching moment coefficient of the wing is $C_M = -0.11$ and the design diving speed is $V_D = 125$ m/s.

Tasks:

a) Determine the manoeuvre *V-n* diagram using the certification requirements CS-23.



- b) Implement a calculation methodology that enables the direct stresses and the shear stresses acting on the skin and spar of the section of Figure 1 to be computed, for the load cases provided and for arbitrary values of t_c , t_a , A_1 , and A_2 . In this methodology the spar flanges can be idealized but not the skin.
- c) Determine the values of t_c , t_a , A_1 e A_2 which minimize the structure mass considering the applied stresses at the root section, the data of Tables 1, 2, and 3 and guaranteeing that the maximum tip deflection is less than 0.1b and that the maximum tip twist angle is less than 2° .
- d) Analise and comment the results.
- e) Write up a technical report.

3. REPORT

Each team of 3 students (each team uses a different value of i from Table 3) must present the methodology and the results of its analysis in a technical written report of **no more than 12 pages**. In the report, adequate detail must be provided concerning the solution steps and the final results, explicitly mentioning the values of t_c , t_a , A_1 e A_2 , the tip deflection, the tip twist, and the stress field over the wing. A critical analysis of the results with proposals for improving the structural efficiency must be provided.

The final hand-in date of the report is <u>12 January</u>, <u>2023</u>. The report must be sent in <u>pdf format</u> to the e-mail address <u>pgamboa@ubi.pt</u>.

4. DATA

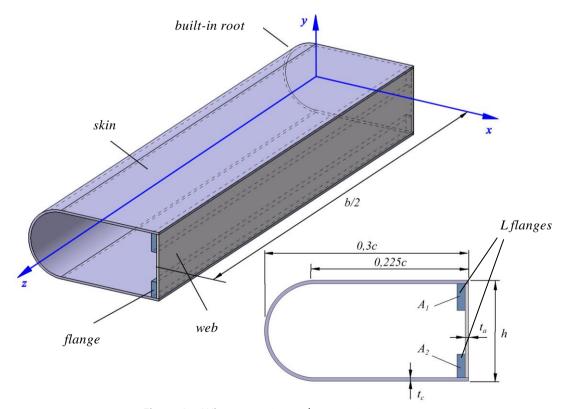


Figure 1 – Wing geometry and parameters.

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Table 1 – Material properties

Property	parameter	unit	7075-T6	2024-T3	6061-T6
Density	ρ	kg/m³	2810	2780	2700
Longitudinal elastic modulus	E	GPa	71.7	73.1	68.9
Poisson ratio	ν	-	0,33	0,33	0,33
Tensile yield stress	$\sigma_{\!\scriptscriptstyle \! Vt}$	MPa	469	345	276
Tensile strength	$\sigma_{\!t}$	MPa	538	483	310
Compression strength	$\sigma_{\!t}$	MPa	514	462	297
Shear strength	au	MPa	331	283	207

Table 2 – Available thicknesses (in mm).

0.122; 0.254; 0.417; 0.61; 0.813; 1.02; 1.22; 1.42; 1.63; 1.83; 2.03; 2.34; 2.95; 4.06; 5.38; 6.4; 8.23; 10.16; 12.7

Table 3 – Wing specifications according to team number.

Team	<i>b</i> , m	<i>c,</i> m	<i>h,</i> m
i = 1,30	11.5-0.01×(i-1)	0.75+0.01×(i-1)	0.15 <i>c</i>

Table 4 – Teams.

		Table 4 Teams.		
Team	Student 1	Student 2	Student 3	
1	Miguel Ruivo - 48147	André Sousa - 48185	Octávio Lopes - 48508	
2	Daniel Câmara - 47795	Fernando Faria - 48082	Raúl Santos - 48558	
3	Henrique Vieira - 47797	Gonçalo Dias - 48008	Luís Lopes - 48808	
4	Weila Fernandes - 44995	Kissange Muthemba - 46713	Ludnesia da Mata - 47093	
5	Diogo Pinho - 47801	Miguel Albino - 47808	Beatriz Gonçalves - 48594	
6	Alexandre Teixeira - 47710	Isabel Gomes - 47822	Pedro Moreira - 48317	
7	Maria Fernandes - 47978	Bernardo Guerreiro - 48428	Pedro Rafeiro - 48683	
8	Pedro Leite - 48141	Mariana Peixoto - 48161	Diogo Garcia - 48587	
9	Duarte Pereira - 47603	Leonardo Santos - 47610	José Miguel Costa - 48214	
10	Mafalda Assis - 48022	Afonso Gamboa - 48261	Anton Mamus - 48618	
11	Guilherme Martins - 48007	Breno Cabral - 48334	Alexandre Pereira - 48502	
12	Sebastião Ventura - 47768	Fernando Afonso - 48175	Francisco Albuquerque - 48220	
13	Ricardo Fonte - 31505	Neusa Panzo - 43082	Christian Delgado - 48824	
14	António Pimenta - 42135	Dany Cardoso - 44605	Gustavo Prado - E11284	
15	Lara Sampaio - 47835	Tomás Carneiro - 47964	Guilherme Rebelo - 48107	
16	André Tomaz - 48108	Cristina Martins - 48392	Rodrigo Silva - 48599	
17	Fábio Teixeira - 45724	Rodrigo Oliveira - 45752	Erik Rosário - 46712	
18	Rui Teixeira - 45442	Francisco Ribeiro - 48089	Inês Afonso - 50191	
19	Bruno Rocha - 40726	João Rosa - 45676	Gonçalo Moreira - 48327	
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