

## Estruturas Aeroespaciais I – 10362

2021/2022

### Mini Project Sizing of a wingbox

#### 1. OBJECTIVE

To size the structure of a wingbox subject to strength and stiffness constraints. To write a technical report.

#### 2. DESCRIPTION

It is required to size the wingbox of an ultralight aircraft which has a maximum take-off mass of  $m = 450$  kg and limit load factors of  $n = +4/-2$ .

A simplified representation of the wing's geometry and the definition of the wingbox parameters are shown in Figure 1. The wingbox has a constant width  $0.3c$ , a constant height  $h$ , and a span  $b$ .

The wingbox structure is made of a closed thin-walled single section. The wingbox skin has thickness  $t_c$  and the spar web has thickness  $t_a$ . The cross-section areas of the upper and lower spar flanges are  $A_1$  and  $A_2$ , respectively. The root of the wing is assumed to be built-in at the main spar and the tip is free. One of two different materials can be used in the design of the wingbox, the aluminium alloys 6061-T6 or 2024-T3, both being isotropic materials with properties given in Table 1. The available thicknesses are given in Table 2.

A first load case to apply to the wing includes a uniformly distributed vertical load,  $w_L$ , along the span corresponding to the wing lift and a uniformly distributed torsion moment,  $w_T$ , along the span. This load system is applied a distance  $0.05c$  in front of the wing spar at the horizontal symmetry axis. A second load case has an upward point force acting on the spar at a distance  $1.5$  m from the wing root. This force represents the ground reaction at the main wheel in a landing condition with a ground load factor  $n_g = 3.5$ .

The maximum lift coefficient of the wing is  $C_{Lmax} = 1.66$ , the minimum negative lift coefficient is  $C_{Lmin} = -C_{Lmax}/2$ , the lift coefficient is given by  $C_L = 0,011\pi^2 b(\alpha+4)/(b+2c)$ , where  $\alpha$  is the angle of attack, the pitching moment coefficient of the wing is  $C_M = -0.1$  and the design diving speed is  $V_D = 86$  m/s.

Tasks:

- Determine the manoeuvre  $V$ - $n$  diagram using the certification requirements CS-VLA.
  - Implement a calculation methodology that enables the direct stresses and the shear stresses acting on the skin and spar of the section of Figure 1 to be computed, for the
-

load cases provided and for arbitrary values of  $t_c$ ,  $t_a$ ,  $A_1$ , and  $A_2$ . In this methodology the spar flanges can be idealized but not the skin.

- c) Determine the values of  $t_c$ ,  $t_a$ ,  $A_1$  e  $A_2$  which minimize the structure mass considering the applied stresses at the root section, the data of Tables 1, 2, and 3 and guaranteeing that the maximum tip deflection is less than  $0.1b$  and that the maximum tip twist angle is less than  $2^\circ$ .
- d) Design the connection between the wing spar and the fuselage considering the loads at the wing root.
- e) Analise and comment the results.
- f) Write up a technical report.

### 3. REPORT

Each team of 3 students (each team uses a different value of  $i$  from Table 3) must present the methodology and the results of its analysis in a technical written report of **no more than 12 pages**. In the report, adequate detail must be provided concerning the solution steps and the final results, explicitly mentioning the values of  $t_c$ ,  $t_a$ ,  $A_1$  e  $A_2$ , the tip deflection, the tip twist, and the stress field over the wing. A critical analysis of the results with proposals for improving the structural efficiency must be provided.

**The final hand-in date of the report is 7 January, 2022. The report must be sent in pdf format to the e-mail address [pgamboa@ubi.pt](mailto:pgamboa@ubi.pt).**

### 4. DATA

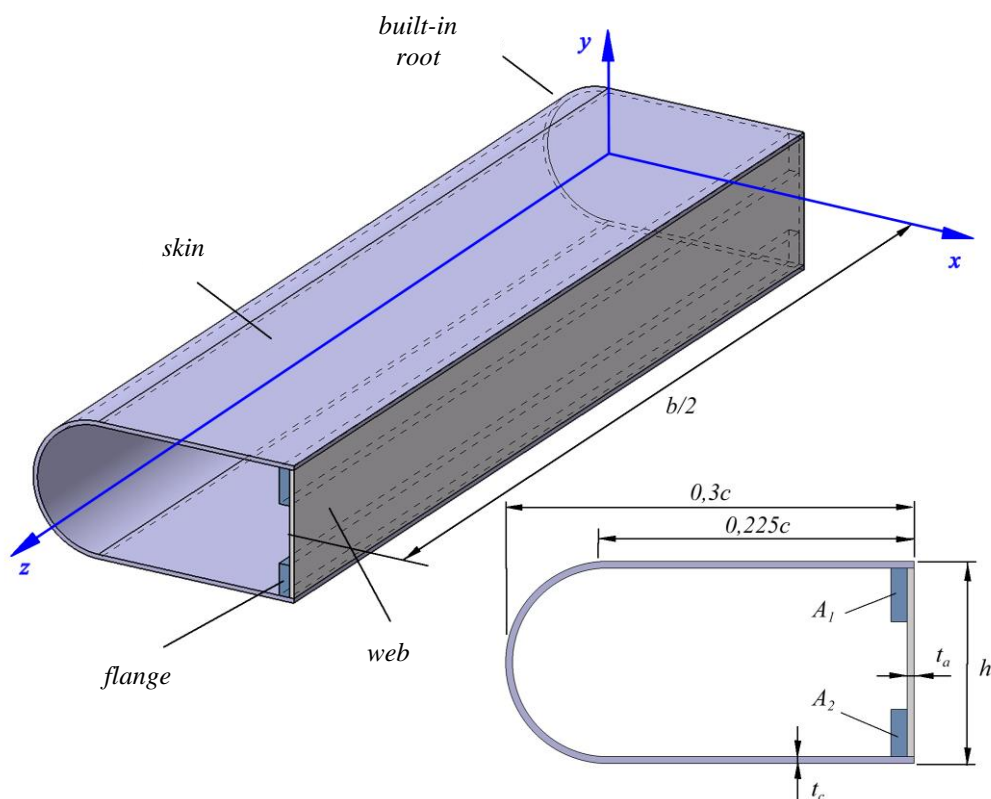


Figure 1 – Wing geometry and parameters.

Table 1 – Material properties

Property	parameter	unit	6061-T6	2024-T3
Density	$\rho$	kg/m <sup>3</sup>	2700	2780
Longitudinal elastic modulus	$E$	GPa	68,9	73,1
Poisson ratio	$\nu$	-	0,33	0,33
Tensile yield stress	$\sigma_{yt}$	MPa	276	345
Tensile strength	$\sigma_t$	MPa	310	483
Compression strength	$\sigma_c$	MPa	297	462
Shear strength	$\tau$	MPa	207	283

Table 2 – Available thicknesses (in mm).

0.122 ; 0.254 ; 0.417 ; 0.61 ; 0.813 ; 1.02 ; 1.22 ; 1.42 ; 1.63 ; 1.83 ; 2.03 ; 2.34 ; 2.95 ; 4.06 ; 5.38 ; 6.4 ; 8.23 ; 10.16 ; 12.7
--

Table 3 – Wing specifications according to team number.

Team	$b$ , m	$c$ , m	$h$ , m
$i = 1,30$	$11.5 - 0.01 \times (i - 1)$	$0.75 + 0.01 \times (i - 1)$	$0.15c$

Table 4 – Teams.

Team	Student 1	Student 2	Student 3
1	Matilde Figueiredo - 43330	Egor Ukolov - 43882	
2	João Barateiro - 43726	João Charuto - 44204	Nuno Souza - 44515
3	Diego Côrte-Real - 43300	Tomás Figueiredo - 43825	Dany Cardoso - 44605
4	Erika Marques - 43418	Rafael Fernandes - 43421	Francisco Costa - 43465
5	Maria Leonor Patricio - 43615	Manuel Azevedo - 44357	Liane Moura - 44473
6	António Pelouro - 45397	Marta Dias - 47088	
7	Vasco Gabriel - 45392	Miguel Sousa - 45402	
8	Rodrigo Silva - 43590	Catarina Oliveira - 43988	Ema Marques - 44070
9	Inês de Medeiros - 44598	Miguel Marques - 44671	
10	Colinet Contreiras - 38883	Edson Varela - 42247	
11	Manuel Matos - 43654	Leonardo Ferreira - 43744	Rafael Rodrigues - 44152
12	Simão Pereira - 43604	Salvador Fernandes - 43748	Diogo Lopes - 44463
13	André Viana - 38593	Diogo Silva - 44099	Hugo Gonçalves - 44198
14	Tiago Nave - 43809	Petro Petrovych - 44040	
15	Francisco Ramos - 43356	António Vilaça - 43693	Rafael Simões - 44069
16	Francisca Serras - 43386	Joana Limpo - 44021	Daniel Pinto - 44963
17	Pedro Cardoso - 43474	Simão Ribeiro - 43823	João Campos - 43854
18	Rimaldini Tavares - 44505	Gilson Lopes - 44636	Jefferson Cardoso - 44655
19	António Duarte - 41977	Bruno Eusébio - 44315	Gonçalo Almeida - 44317
20			
21			
22			
23			
24			
25			
26			
27			
28			
29			